



TMR-0012

2

AD

Reports Control Symbol  
OSD - 1366

AD-A252 110



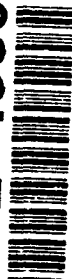
DEVELOPMENT OF MESOSCALE MODEL PERFORMANCE  
EVALUATION PROGRAMS

DTIC  
ELECTE  
JUN 17 1992  
S A D

April 1992

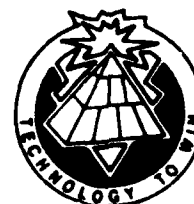
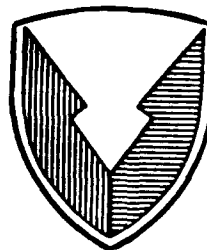
Teizi Henmi  
Roger Vega

92-15605



92 6 1 134

Approved for public release; distribution is unlimited.



US ARMY  
LABORATORY COMMAND

ATMOSPHERIC SCIENCES LABORATORY  
White Sands Missile Range, NM 88002-5501

## NOTICES

### Disclaimers

The findings in this report are not to be construed as an official Department of the Army position, unless so designated by other authorized documents.

The citation of trade names and names of manufacturers in this report is not to be construed as official Government indorsement or approval of commercial products or services referenced herein.

### Destruction Notice

When this document is no longer needed, destroy it by any method that will prevent disclosure of its contents or reconstruction of the document.

REPORT DOCUMENTATION PAGE			Form Approved OMB No 0704-0188	
<small>Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.</small>				
1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE April 1992	3. REPORT TYPE AND DATES COVERED Final	
4. TITLE AND SUBTITLE  Development of Mesoscale Model Performance Evaluation Programs			5. FUNDING NUMBERS  TA: 62784-AH71-D	
6. AUTHOR(S)  Teizi Henmi and Roger Vega				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)  U.S. Army Atmospheric Sciences Laboratory White Sands Missile Range, NM 88002-5501			8. PERFORMING ORGANIZATION REPORT NUMBER  ASL-TMR-0012	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES)  U.S. Army Laboratory Command Adelphi, MD 20783-1145			10. SPONSORING / MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES				
12a. DISTRIBUTION / AVAILABILITY STATEMENT  Approved for public release; distribution is unlimited.			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words)  Computer programs to examine and illustrate the results of mesoscale model simulation and to compare with observation are described. Programs consist of those illustrating horizontal and vertical measurements and temporal distributions of both simulated and observed data. Statistical methods to evaluate model performance are also programmed.				
14. SUBJECT TERMS  mesoscale model, model evaluation method			15. NUMBER OF PAGES 37	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT SAR	

# CONTENTS

LIST OF FIGURES.....	4
1. INTRODUCTION.....	7
2. PROJECT WIND DATA AND MODEL SIMULATION.....	7
3. DATA INTERPOLATION METHODS.....	8
3.1 Upper-Air Data.....	8
3.2 Surface Data.....	9
4. SURFACE METEOROLOGICAL PARAMETERS.....	9
4.1 Horizontal Distributions of Gridded Data.....	9
4.2 Comparisons of Simulation with Surface Observation.....	10
5. UPPER-AIR METEOROLOGICAL PARAMETERS.....	10
5.1 Vertical Distributions at the Locations of Sounding Stations....	10
5.2 Time-Series at Different Levels.....	11
6. EVALUATION OF MODEL PERFORMANCE.....	11
6.1 Surface Data.....	12
6.2 Upper-Air Data.....	13
7. CONCLUDING REMARKS.....	14
LITERATURE CITED.....	37
DISTRIBUTION LIST.....	39



Accession For	
NTIS CPASI	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By	
Distribution /	
Availability Codes	
Dist	Avail and/or Special
A-1	

## LIST OF FIGURES

1.	Project WIND terrain map, with 400 m height contours.....	15
2.	Interpolation method of vertical data.....	16
3.	Temperature distribution with 5 °C contours.....	17
4.	Sensible heat flux distribution over terrain data--solid lines for upward flux and broken lines for downward flux.....	18
5.	Horizontal wind vector distributions--right side for simulation and left side for observation--maximum arrow = 7.35 m/s.....	19
6.	Comparison of surface data--thin lines for simulation and thick lines for observation, wind direction, and windspeed--temperatures at 2- and 10-m levels, dew point, and downward shortwave radiation as a function of time for station S1.....	20
7.	Comparison of surface data--thin lines for simulation and thick lines for observation, wind direction, and windspeed--temperatures at 2- and 10-m levels, dew point, and downward shortwave radiation as a function of time for station C1.....	21
8.	Vertical distributions of wind direction and windspeed, and hori- zontal components of wind vectors, temperature, and dew point--thin lines for simulation and thick lines for observation.....	22
9.	Vertical distributions of wind direction and windspeed, and hori- zontal components of wind vectors, temperature, and dew point--thin lines for simulation and thick lines for observation.....	23
10a.	Time series of wind direction and windspeed at 800-, 400-, and 200-m levels for station = 03.....	24
10b.	Time series of wind direction and windspeed at 100-, 50-, and 10-m levels for station = 03.....	25
11a.	Time series of temperature and dew point at 800-, 400-, and 200-m levels for station = 03.....	26
11b.	Time series of temperature and dew point at 100-, 50-, and 10-m levels for station = 03.....	27
12.	Time series of wind direction and windspeed at 500-, 700-, 850-mbar levels for station = 03.....	28
13.	Time series of temperature and dew point at 500-, 700-, and 850-mbar levels for station = 03.....	29

14.	Time series of statistical parameters for surface wind data.....	30
15.	Time series of statistical parameters for surface (10-m level) temperature.....	31
16.	Time series of average differences between observation and simulation for horizontal wind vector components, speed, temperature, dew point, and pressure at the 10-m level.....	32
17.	Time series of average differences between observation and simulation for horizontal wind vector components, speed, temperature, dew point, and pressure at the 1000-m level.....	33
18.	Time series of correlation coefficients of horizontal wind vector components, speed, temperature, dew point, and pressure for the 10-m level.....	34
19.	Time series of correlation coefficients of horizontal wind vector components, speed, temperature, dew point, and pressure for the 1000-m level.....	35

## 1. INTRODUCTION

In 1992, the U.S. Army will sponsor the workshop on mesoscale model technology exchange. The workshop will be handled by the MESOMET Panel. The objectives of the workshop are the following:\*

- to identify state-of-the-art technology of mesoscale modeling;
- to inform the scientific community about the availability of Project WIND (wind in non-uniform domains) data; and
- to serve as a forum for mesoscale modeling technology exchange.

The U.S. Army Atmospheric Sciences Laboratory (ASL) will be assigned to examine the subset of the outputs that are generated by eight different mesoscale models.

In the last several months, several computer programs to examine and display the outputs of the mesoscale model to compare with observations, have been developed by ASL using the output of a mesoscale model HOTMAC (High Order Turbulence Model for Atmospheric Circulation) (Yamada and Bunker, 1989) and Project WIND Phase I, Julian days 178-179, data (Cionco, 1990). Programs developed consist of those displaying horizontal, vertical, and temporal distributions of meteorological parameters--simulated and observed.

This report describes the methods used to examine model output and show examples of graphic display. Detailed results of comparisons between model simulation and observation will be described in the near future. The computer programs are developed by using the FORTRAN language with the National Center for Atmospheric Research (NCAR) GKS-Compatible Graphic System. The programs are on the HP 9000/840 computer at ASL.

## 2. PROJECT WIND DATA AND MODEL SIMULATION

Data used to develop the program was from Project WIND Phase I, covering 24 h from 0900 l.s.t. of day 178. These measurements consisted of upper-air sounding data at five locations every 2 h, with a few missing data, and 21 surface station data. Details of the data set are presented in Cionco (1990).

Model simulation was conducted over terrain as shown in figure 1.\*\* Latitude and longitude of the southwestern corner of the domain are  $39^{\circ} 11' 04.4''$  N and  $122^{\circ} 59' 58''$  W. The terrain heights were represented by grids of 81 by 81 with a unit grid distance of 2.5 km. The highest and lowest grid points are 2477 and 12 m, respectively, above sea level. In the figure, numbers represent the locations of upper-air stations. Meteorological parameters were calculated at every other grid point (40 by 40) for 16 vertical layers, using HOTMAC. The model was initialized at 0900 l.s.t. of day 178 using sounding data taken at station 04, and simulation continued until 0800 l.s.t. of the next day.

---

\*J. E. Harris and R. E. Meyers, 1991, Trip report on meeting of MESOVET Panel in Bruges, Belgium, 9-10 May 1991 (unpublished).

\*\*Figures are presented at the end of the text.

In figure 1b the locations of surface observations are marked. Surface data contained windspeed, wind direction, temperature, relative humidity, pressure, incoming solar radiation, and precipitation. During the 24-h period (between 0900 l.s.t. of day 178 and 0900 l.s.t. of day 179), no precipitation occurred. Therefore, precipitation data was not examined. Relative humidity data was converted to dew point by using empirical formulas.

### 3. DATA INTERPOLATION METHODS

#### 3.1 Upper-Air Data

Generally, most mesoscale models are formulated on terrain-following coordinates, and meteorological parameters are calculated at particular heights determined by model design. To compare model output with observation at a desired height, one must interpolate both model outputs and observed data to the height. Model output values computed at a grid point most adjacent to an upper-air sounding station were used for the comparison study.

In HOTMAC model, the following equation is used to define a terrain-following vertical coordinate.

$$z^* = \bar{H} \frac{z - z_g}{H - z_g} \quad (1)$$

where  $z^*$  and  $z$  are the transformed and Cartesian vertical coordinates, respectively;  $z_g$  is ground elevation above sea level;  $\bar{H}$  is the material surface top of the model; and  $H$  is the corresponding height in the coordinate. For simplicity,  $H$  is specified as

$$H = \bar{H} + z_{gmax} \quad (2)$$

where  $z_{gmax}$  is the maximum value of  $z_g$ . From equation (1), height above ground  $H_g$  can be given as

$$H_g = z - z_g = z^* \frac{\bar{H} + z_{gmax} - z_g}{\bar{H}} \quad (3)$$

The author applied both linear interpolation and cubic spline methods to interpolate the values of meteorological parameters (horizontal wind components, temperature, and dew point) at desired height above ground. Few differences were found in the results produced by the two methods. In the linear interpolation method, meteorological parameter  $\varphi$  at height  $z$  can be obtained by using the values at  $z_i$  and  $z_{i+1}$ , where  $z_i < z < z_{i+1}$ , as follows: (figure 2)

$$\varphi(z) = A \cdot \varphi_i + B \cdot \varphi_{i+1} \quad (4)$$

where



$$A = \frac{z_{i+1} - z}{z_{i+1} - z_i} \quad (5)$$

$$B = \frac{z - z_i}{z_{i+1} - z_i} \quad (6)$$

The equation for cubic spline interpolation is expressed as

$$\varphi(z) = A \cdot \varphi_i + B \cdot \varphi_{i+1} + C \cdot \varphi''_i + D \cdot \varphi''_{i+1} \quad (7)$$

where

$$C = \frac{1}{6} \cdot (A^3 - A) \cdot (z_{i+1} - z_i)^2 \quad (8)$$

$$D = \frac{1}{6} \cdot (B^3 - B) \cdot (z_{i+1} - z_i)^2 \quad (9)$$

and

$$\varphi'' = \frac{d^2 \varphi}{dz^2} \quad (10)$$

FORTTRAN programs of cubic spline interpolation described in Press et al. (1989) were used.

### 3.2 Surface Data

To reduce the value of a meteorological parameter at a surface station  $k$ , values at four grid points surrounding the station were used as

$$\varphi_k = \frac{\sum_i \varphi_i \frac{1}{r_i^2}}{\sum_i \frac{1}{r_i^2}} \quad (11)$$

where the subscript  $i$  represents a grid point,  $r_i$  is the distance between station location and grid point  $i$ , and  $\varphi$  is an arbitrary meteorological parameter.

## 4. SURFACE METEOROLOGICAL PARAMETERS

### 4.1 Horizontal Distributions of Gridded Data

Plotting horizontal distributions of gridded data of model output is important to examine distribution patterns of meteorological parameters over the model

domain and to intercompare between models. Scalar variables such as temperature and sensible heat flux are plotted by using contour-line drawing routines in the NCAR GKS-Compatible Graphic System. Horizontal wind vectors are plotted by using vector drawing routines. In the following figures, (a) and (b) represent daytime and nighttime conditions for 1500 l.s.t. of day 178 and 0300 l.s.t. of day 179, respectively.

Examples of contour-line plotting of scalar variables are shown in figures 3 and 4. Figures 3a and 3b show air temperature distributions at 10-m levels above ground. Contour lines are drawn with 5 °C intervals. Terrain contour lines are also drawn using thin lines. Figure 4 shows the distribution of sensible heat flux ( $W/m^2$ ). Sensible heat fluxes are upward (positive) throughout the model domain during the day, and downward (negative) during the night. Upward fluxes are contoured by solid lines and downward fluxes by broken lines.

Figure 1b shows that surface observation stations were in the center of the model domain. For easier comparison, the right side of figures 5a and 5b show the horizontal wind vectors computed by the model for the center area only; the left side shows the observed wind vectors. Upslope wind conditions during the day and downslope wind conditions during the night were well simulated and in good agreement with observations.

#### 4.2 Comparisons of Simulation with Surface Observation

The computer program developed for comparing simulation with surface observation takes the following steps:

- determines the locations of surface station in grid coordinate.
- creates time series arrays of meteorological parameters for points representing surface stations, using data at four grid points surrounding the surface stations.

The program is designed to plot both simulation and observation for any surface station desired.

Since the model output file contained hourly data at grid points, time series plotting of both simulated and observed data were also made hourly. Wind direction and windspeed (meters per second), temperatures (degrees Celsius) at 2- and 10-m levels, dew point (degrees Celsius), and downward shortwave radiation (watts per square meter) were plotted. As examples, plottings for stations S1 and C1 are shown, respectively, in figures 6 and 7, with thin lines representing simulation and thick lines representing observation. These figures show that shortwave radiation observation data and temperatures at either level were not available at some stations.

### 5. UPPER-AIR METEOROLOGICAL PARAMETERS

#### 5.1 Vertical Distributions at the Locations of Sounding Stations

Upper-air data were observed at five stations during the 24-h period. Data were taken at each station every 2 h, with some exceptions. The program developed to plot vertical distributions of meteorological parameters extracts data at grid

points closest to the stations and creates arrays of data for each station. The program was arranged so plotting could be made for a desired station and time.

Figure 8 shows the vertical distributions of wind direction and windspeed, x and y components of wind vector, temperature, and dew point for station 01 and 1300 l.s.t. of day 178. Thin and thick lines represent, respectively, simulation and observation. Figure 9 shows station 04 at 0100 of day 179.

## 5.2 Time-Series at Different Levels

For comparison between different models, it is convenient to have meteorological parameters at the same heights. Participants in the workshop of mesoscale model technology exchange are asked to produce time series of meteorological parameters at the following: standard heights 2, 10, 50, 100, 200, 400, 800 m above the ground and standard pressure levels of 850, 700, 500, and 300 mbar. The HOTMAC model computed variables at the following 16 levels of terrain-following coordinates: 0, 2, 6, 10, 14, 28, 114, 281, 530, 861, 1273, 1767, 2342, 3000, 3729, 4559. Thus, interpolation of variables from model height to standard height was necessary. As described in section 3, a cubic spline interpolation method was used for interpolation from model heights to standard heights. The linear interpolation method was used to interpolate to standard pressure level. In the HOTMAC model, pressure is a diagnostic variable.

The program extracts parameters for grid points most adjacent to upper-air stations and calculates the values at standard heights or pressure levels. Observed data were also interpolated by using cubic spline or linear interpolation methods. Time series arrays of meteorological parameters for different station locations and standard levels were generated; therefore, time series of plotting could be easily made for different stations and levels. Wind direction and windspeed, temperature, and dew point were plotted.

Figures 10a and 10b show the time series of wind direction and windspeed at seven different heights for station 03. Continuous lines are used for simulation and asterisks (\*) are used to plot the values of observation. Figures 11a and 11b show examples of the time series of temperature and dew point.

Time series for three different pressure levels (500, 700, and 850 mbar) are given in figures 12 and 13. Neither observation nor simulation was available at the 300-mbar level. Plots for station 03 were used for these figures.

## 6. EVALUATION OF MODEL PERFORMANCE

Visual comparisons of simulation with observations (as shown in the previous sections) are useful. However, model performance evaluated quantitatively is also desirable since it enables us to compare objectively one model to another model and to gain insight into the sources of error. For the present simulation, continuous data of wind direction, windspeed, temperature, and humidity were available throughout the 24-h period at 21 surface stations; and 4 or 5 upper-air sounding data were available every 2 h. These data were used to perform the following statistical evaluations.

### 6.1 Surface Data

Mean, standard deviation, root mean square errors (rmse), unbiased rmse, and agreement measure were calculated hourly. Willmott (1981, 1982) and Willmott et al. (1985) recommend the use of the above statistical parameters to quantitatively evaluate model performance. The following equations are definitions of these parameters:

a. mean

$$\bar{\varphi} = \frac{\sum_k \varphi(k)}{N} \quad (12)$$

where  $\varphi(k)$  is meteorological parameters at kth station, and N is the number of stations. Means for both simulation and observation were calculated. In a good agreement case, means for both should have similar values.

b. rmse (E) and unbiased rmse ( $E_{ub}$ )

$$E = \left\{ \frac{\sum_k [\varphi_m(k) - \varphi_o(k)]^2}{N} \right\}^{1/2} \quad (13)$$

$$E_{ub} = \left\{ \sum_k \frac{[(\varphi_m(k) - \bar{\varphi}_m) - (\varphi_o(k) - \bar{\varphi}_o)]^2}{N} \right\}^{1/2} \quad (14)$$

If there is a perfect agreement, E and  $E_{ub}$  are zero.

c. standard deviation

$$\sigma = \left\{ \sum_k \frac{[\varphi(k) - \bar{\varphi}]^2}{N} \right\}^{1/2} \quad (15)$$

In a good agreement case, the standard deviation for both simulation and observation should have similar values.

d. agreement measure

$$A = 1 - \frac{\sum_k (\varphi_m(k) - \varphi_o(k))^2}{\sum_k (|\varphi_m(k) - \bar{\varphi}_m| + |\varphi_o(k) - \bar{\varphi}_o|)^2} \quad (16)$$

This dimensionless index has a theoretical range of 1.0 (for perfect agreement) to 0.0 (for no agreement).

These statistical parameters were calculated hourly for wind, temperature, and dew point. Figure 14 shows the results for wind. Mean wind direction was calculated from the means of horizontal wind components. Thin lines represent simulation and thick lines represent observation in the top three portions of figure 14. In the rmse plotting,  $E_b$  was drawn using a thin line and  $E_{ub}$  by using a thick line. Agreement measure of windspeed was slightly lower during the day-time than during the night, as mean windspeed showed greater discrepancies during the day than during the night.

Figure 15 is a similar figure for temperature at the 10-m level. There is a good agreement between simulation and observation during the day, as can be seen in mean temperature and agreement measure. Agreement becomes poor during the night, as the standard deviation of observed temperature is much greater than that of simulation during the night, probably resulting from the model's incapability of representing localized effects. The rmse shows also that agreement between simulation and observation becomes poor during the night.

## 6.2 Upper-Air Data

So far, for upper-air data, the following two statistical parameters were calculated at different levels as a function of time to evaluate model performance. Different statistical parameters may need further consideration.

- a. average difference between observation and simulation

$$\overline{\delta\varphi(t)} = \frac{\sum_k |\varphi_{k,o}(t) - \varphi_{k,m}(t)|}{N} \quad (17)$$

where  $\varphi$  represents meteorological parameters, subscripts o and m are for observation and simulation, and N is the number of observations.  $\delta\varphi$  of horizontal wind components, speed, temperature, dew point, and pressure were calculated at different levels every 2 h when observation of upper-air was available. Figures 16 and 17 are for the 10- and 1000-m levels, respectively. At the 10-m level, the difference of temperature becomes greater during the night, as has been mentioned in section 6.1. On the other hand, temperature difference at the 1000-m level did not show great difference at night, probably because temperature at the 1000-m level was influenced very little by surface heating and cooling. The average difference of the x component of wind at the 1000-m level grew after several hours of simulation. In this simulation, the model was initialized at 0900 l.s.t. using upper-air sounding data, and no adjustment was made during simulation.

b. correlation coefficient of variance

$$r(t) = \frac{\sum_k (\delta\varphi'_{k,o} \cdot \delta\varphi'_{k,m})}{\left(\sum_k \delta\varphi_{k,o}^2\right)^{1/2} \cdot \left(\sum_k \delta\varphi_{k,m}^2\right)^{1/2}} \quad (18)$$

where

$$\delta\varphi_o(t + \Delta t) = \varphi_o(t + \Delta t) - \varphi_o(t) \quad (19)$$

$$\delta\varphi_m(t + \Delta t) = \varphi_m(t + \Delta t) - \varphi_m(t) \quad (20)$$

$$\delta\varphi_o' = \delta\varphi_o - \overline{\delta\varphi_o} \quad (21)$$

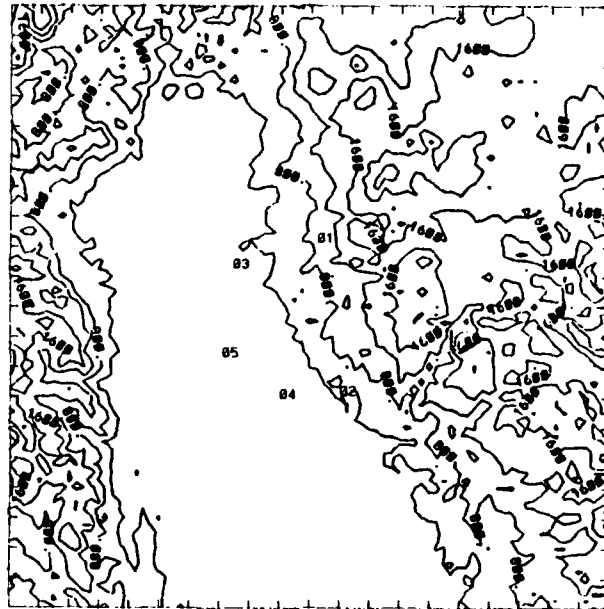
$$\delta\varphi_m' = \delta\varphi_m - \overline{\delta\varphi_m} \quad (22)$$

Here the overline denotes an average of an entire simulation period. The use of the correlation coefficient of variance was suggested by the MESOMET panel.

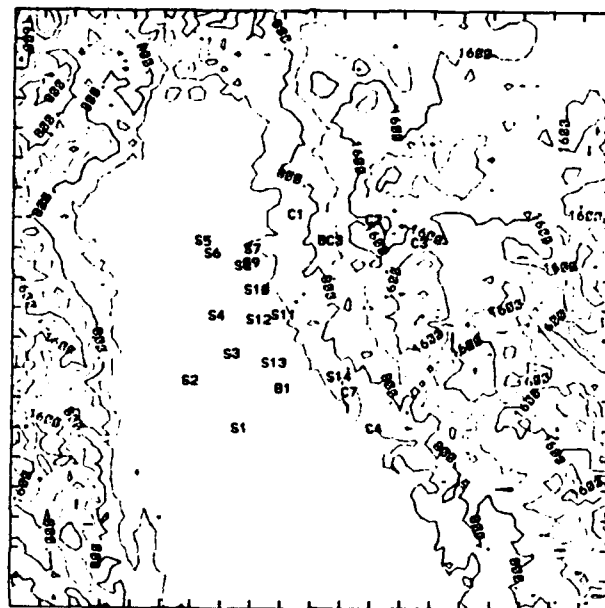
The coefficient  $r(t)$  was calculated for meteorological parameters including horizontal wind components, windspeed, temperature, dew point, and pressure at different levels. Figures 18 and 19 show the 10- and 1000-m levels, respectively. The values of  $r(t)$  vary considerably for all the meteorological parameters. Ideas on model performance are difficult to obtain from these figures. The correlation coefficient must be done carefully.

## 7. CONCLUDING REMARKS

This report describes and illustrates computer programs developed for a comparison between model simulation and observation by using Project WIND Phase I day 178 data and the HOTMAC model output. Temporal and spatial comparisons of simulation with observation can be made by using the program developed. Statistical parameters described in the report will become meaningful when different model simulations are compared with observations.



(a) Locations of upper-air sounding stations, marked with numerical numbers.



(b) Locations of surface stations.

Figure 1. Project WIND terrain map, with 400 m height contours.

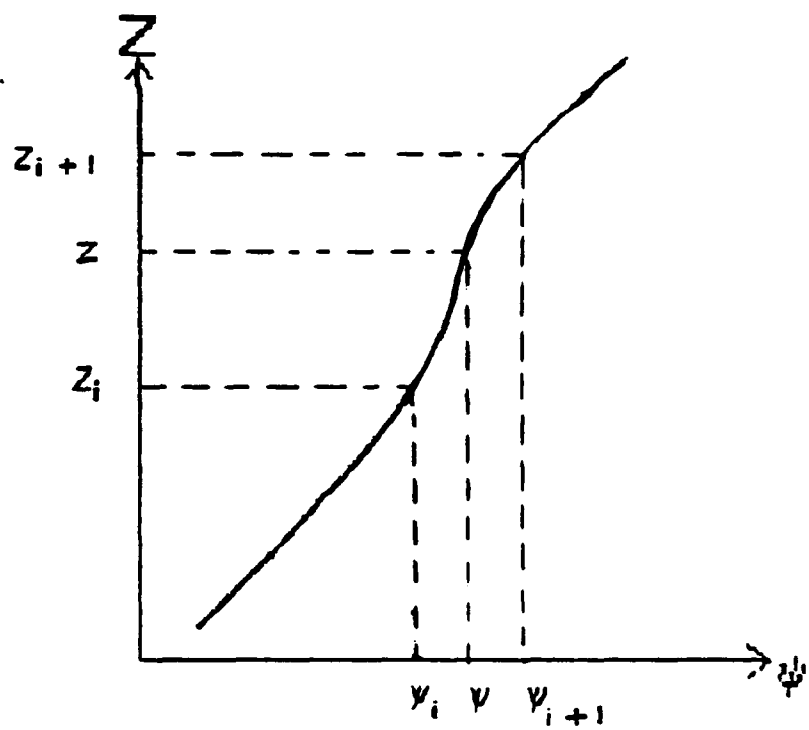
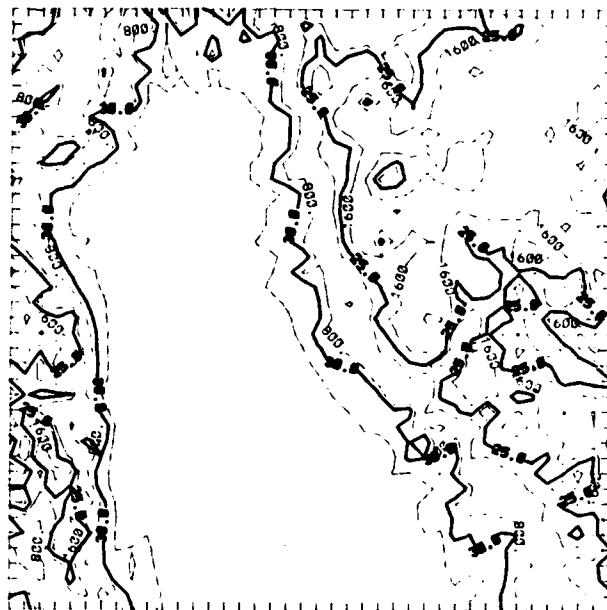
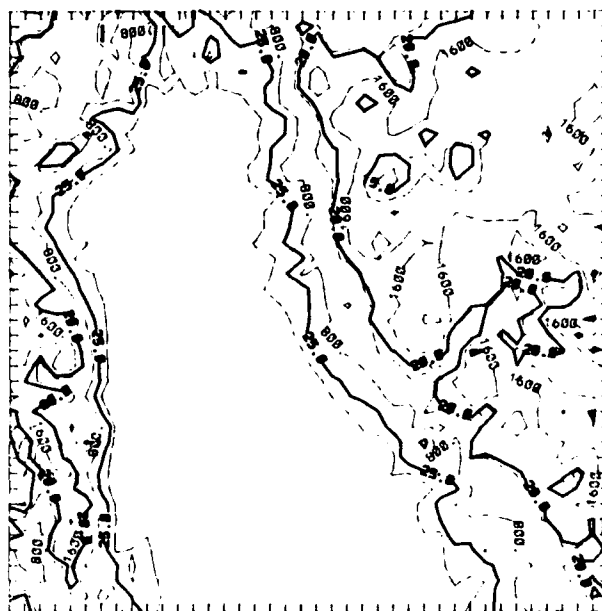


Figure 2. Interpolation method of vertical data.



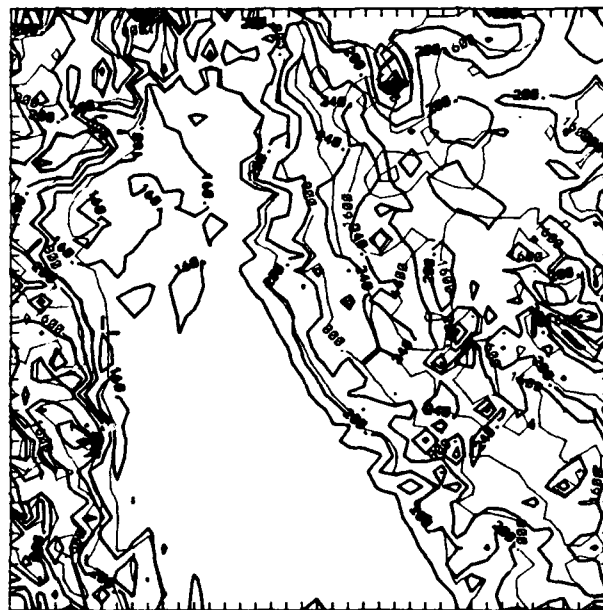


(a) 1500 l.s.t., day 178

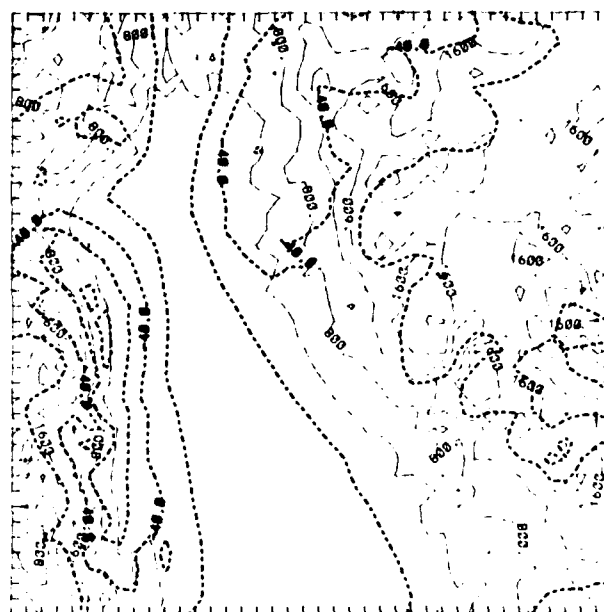


(b) 0300 l.s.t., day 179

Figure 3. Temperature distribution with 5 °C contours.

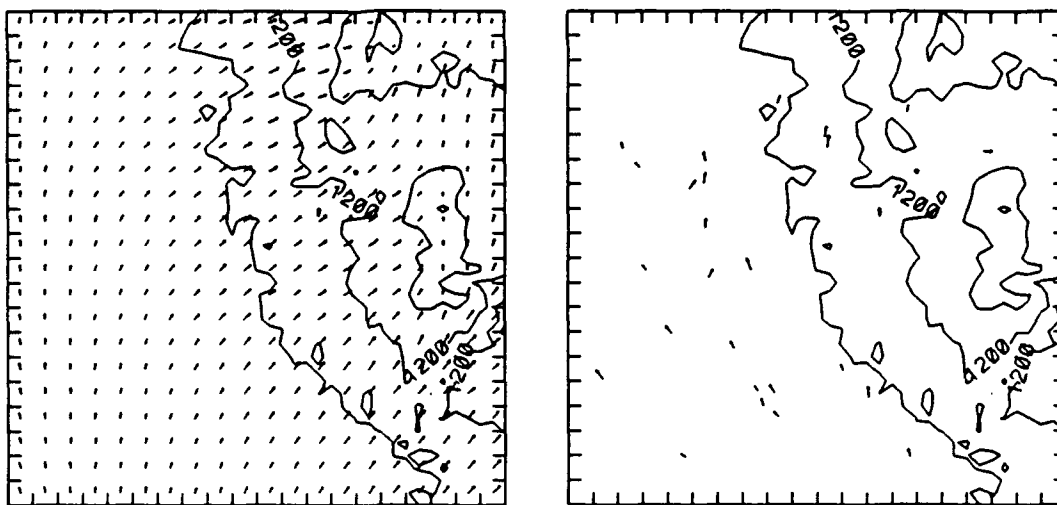


(a) 1500 l.s.t., day 178

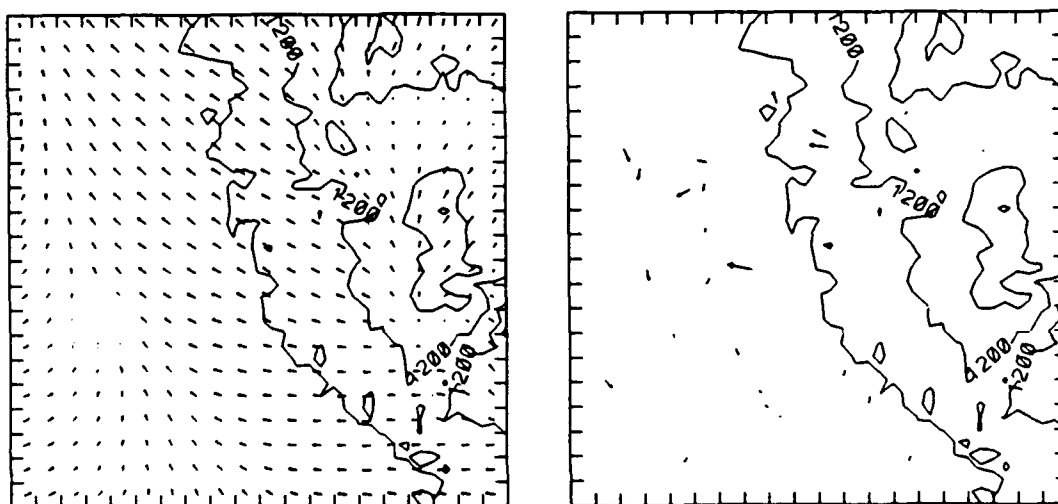


(b) 0300 l.s.t., day 179

Figure 4. Sensible heat flux distribution over terrain data--solid lines for upward flux and broken lines for downward flux.



(a) 1500 l.s.t., day 178



(b) 0300 l.s.t., day 179

Figure 5. Horizontal wind vector distributions--right side for simulation and left side for observation--maximum arrow = 7.35 m/s.

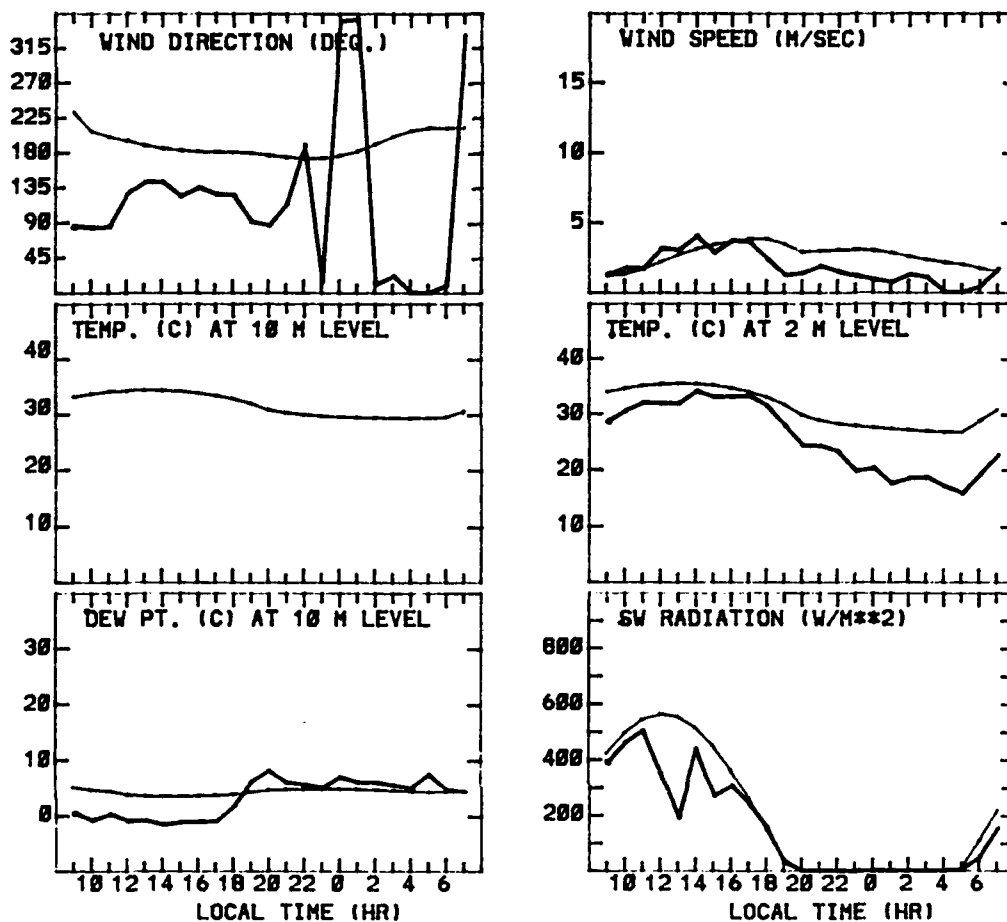


Figure 6. Comparison of surface data--thin lines for simulation and thick lines for observation, wind direction, and windspeed--temperatures at 2- and 10-m levels, dew point, and downward shortwave radiation as a function of time for station S1.

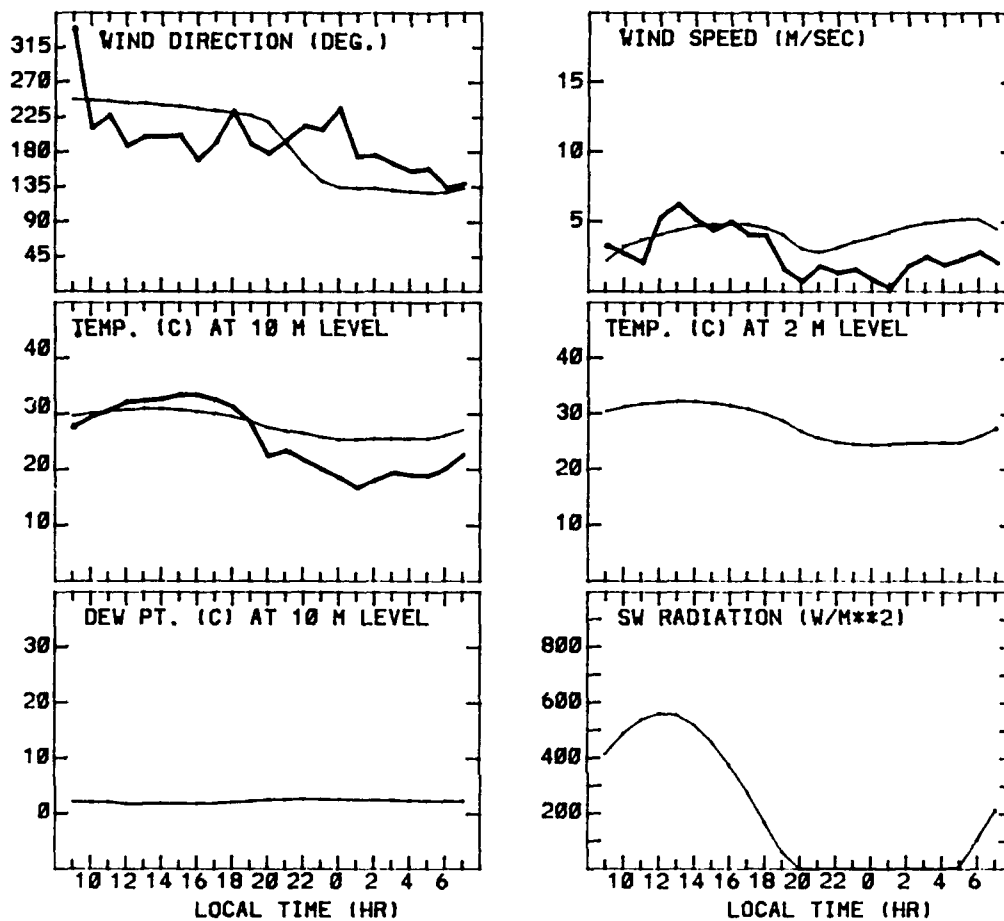


Figure 7. Comparison of surface data--thin lines for simulation and thick lines for observation, wind direction, and windspeed--temperatures at 2- and 10-m levels, dew point, and downward shortwave radiation as a function of time for station C1.

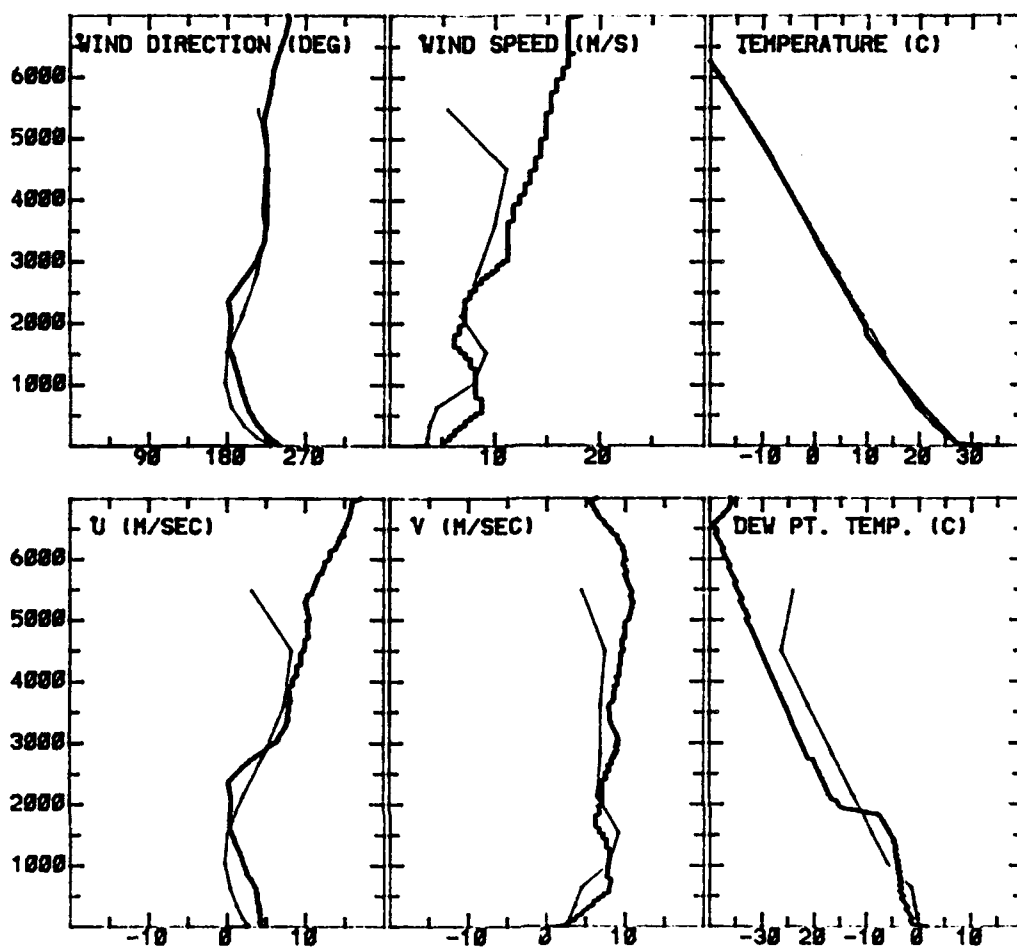


Figure 8. Vertical distributions of wind direction and windspeed, and horizontal components of wind vectors, temperature, and dew point--thin lines for simulation and thick lines for observation. Station = 0.1, 1300 l.s.t., day 178.

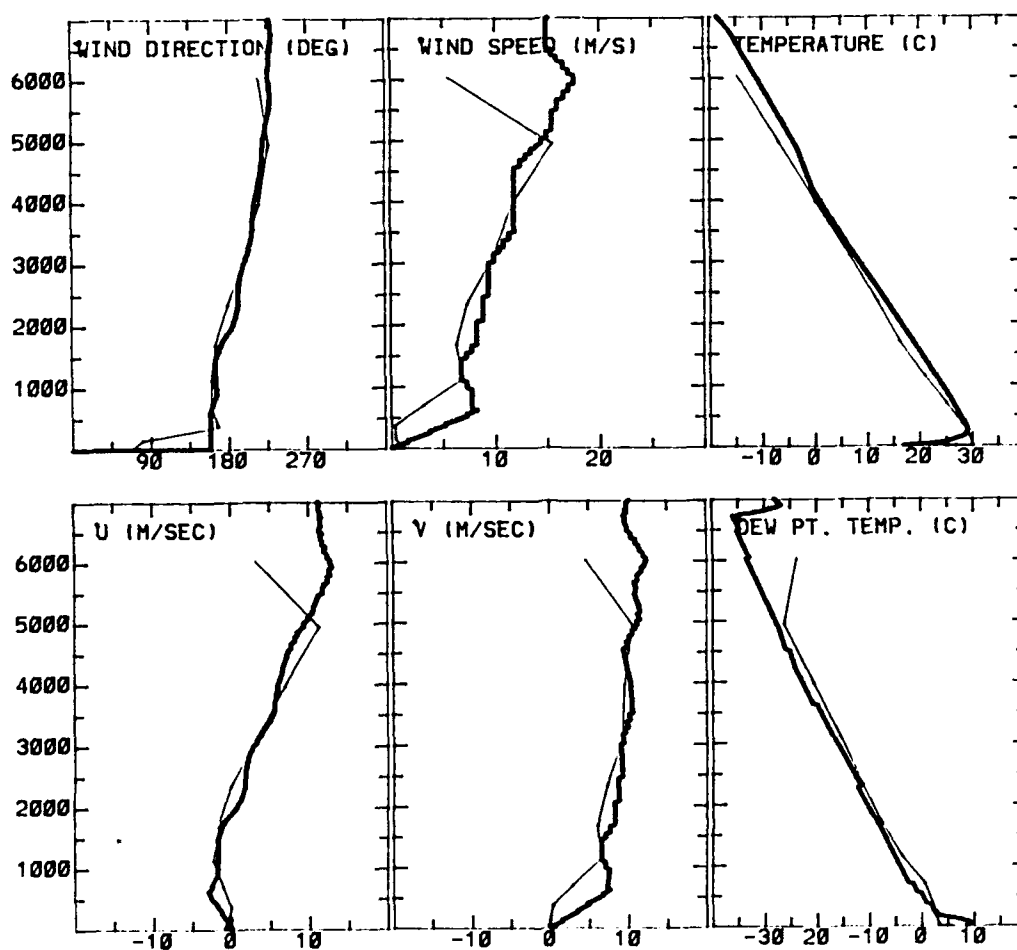


Figure 9. Vertical distributions of wind direction and windspeed, and horizontal components of wind vectors, temperature, and dew point--thin lines for simulation and thick lines for observation. Station = 04, 0100 l.s.t., day 179.

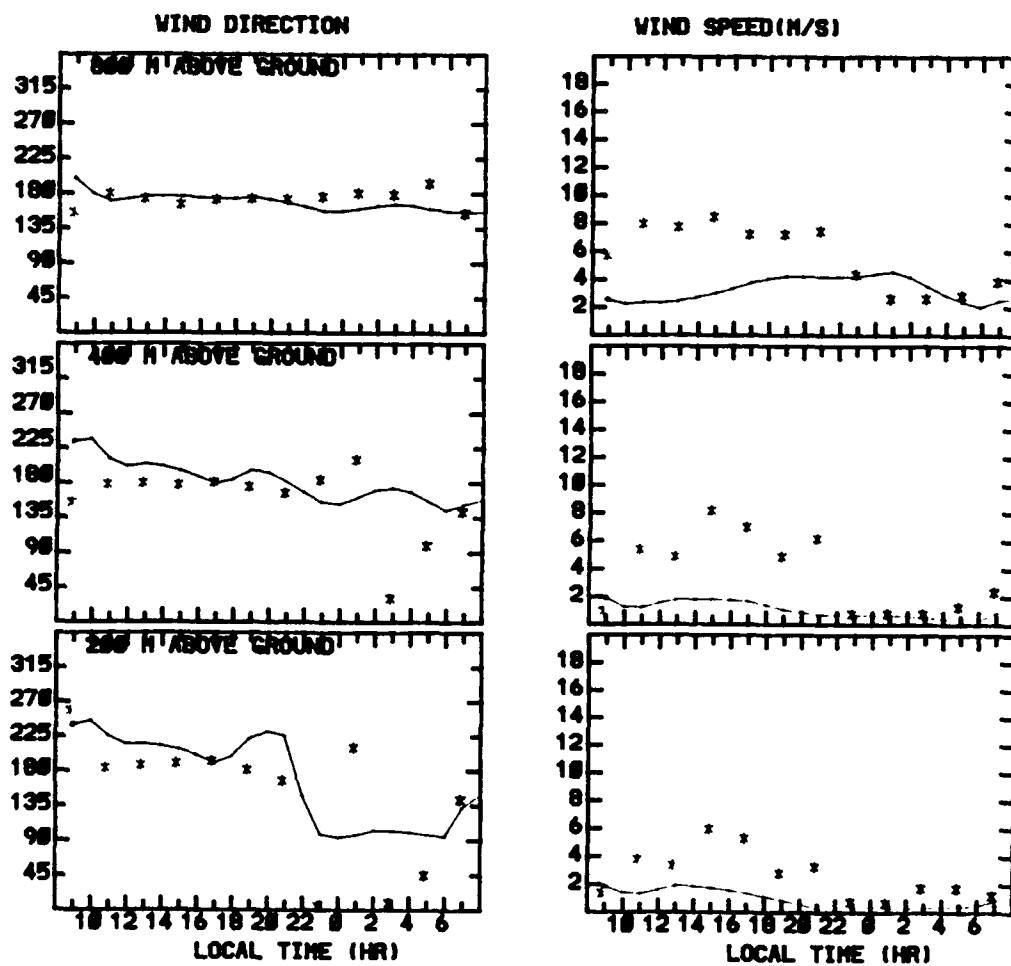


Figure 10a. Time series of wind direction and windspeed at 800-, 400-, and 200-m levels for station = 03.



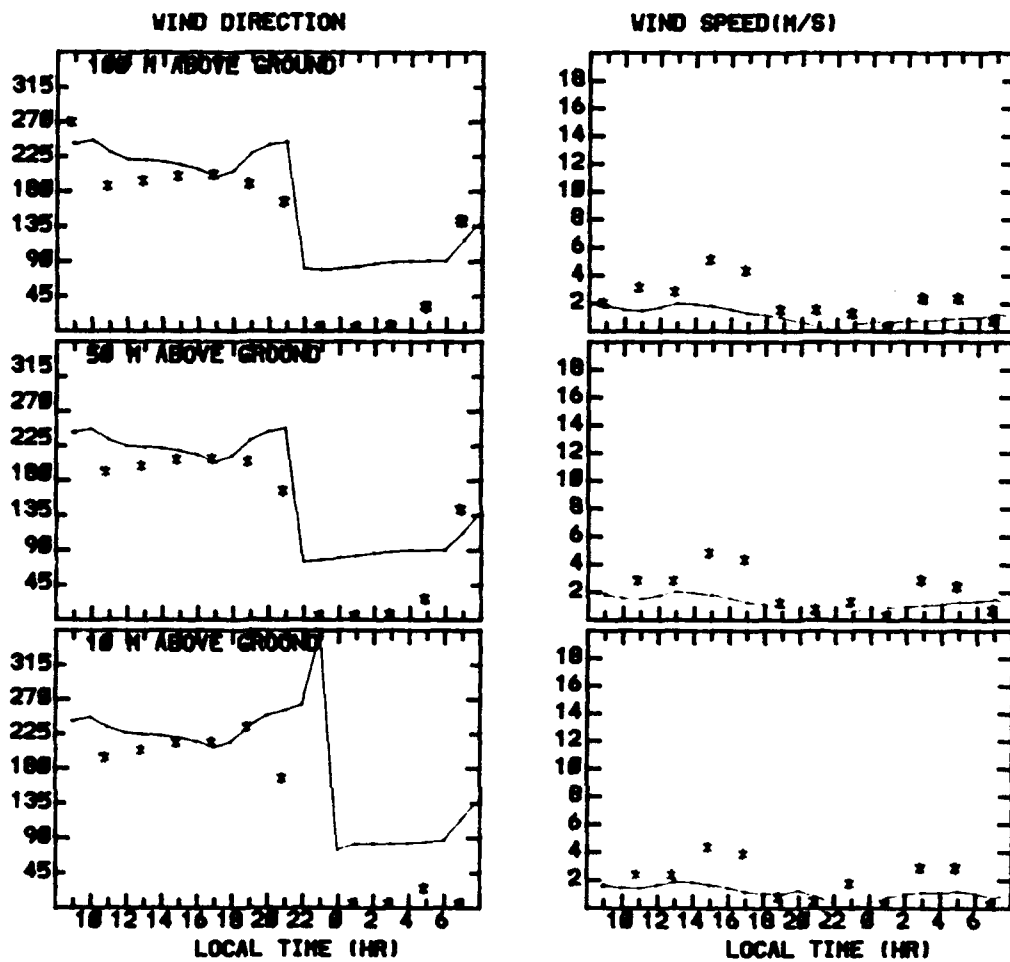


Figure 10b. Time series of wind direction and windspeed at 100-, 50-, and 10-m levels for station - 03.

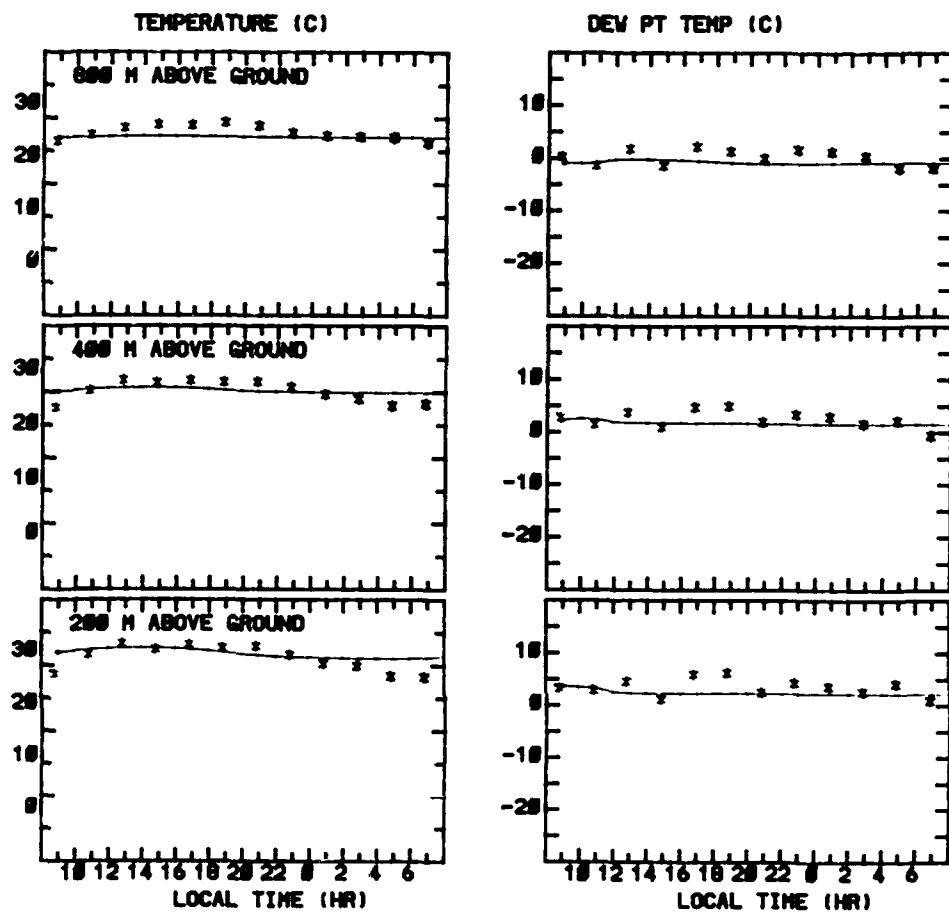


Figure 11a. Time series of temperature and dew point at 800-, 400-, and 200-m levels for station = 03.

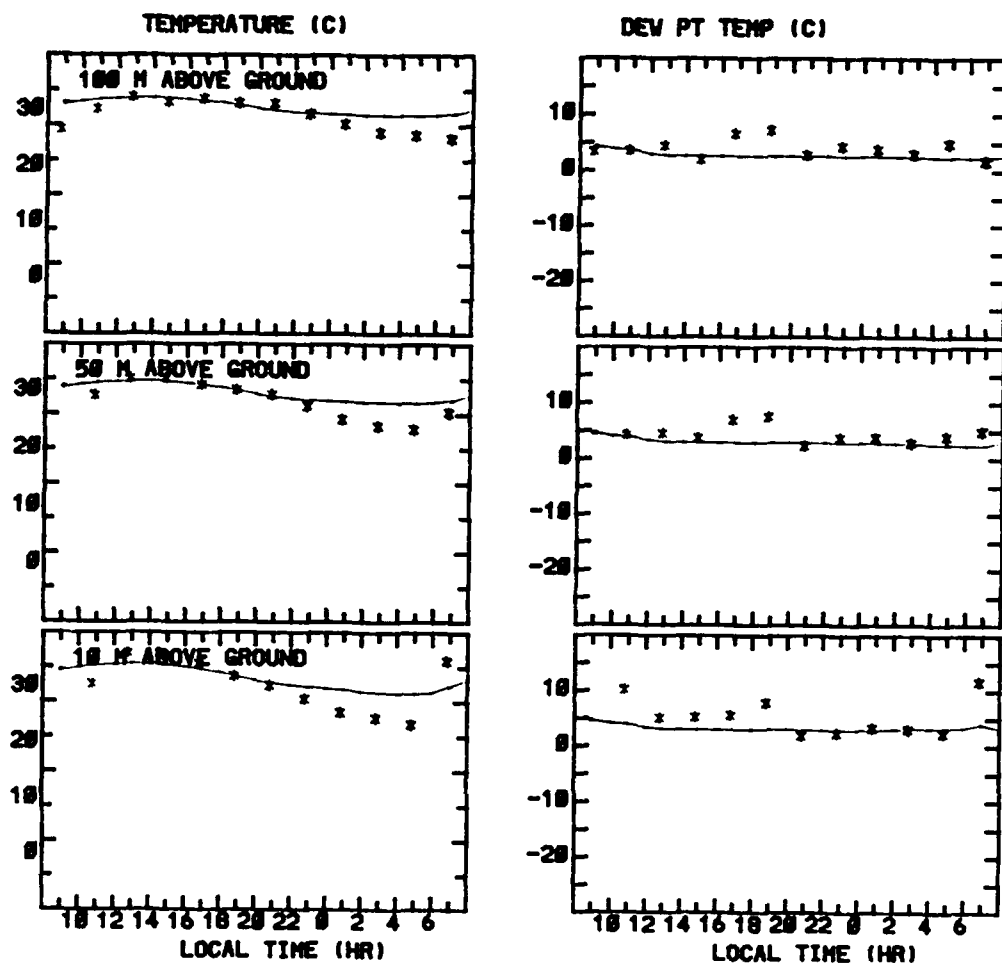


Figure 11b. Time series of temperature and dew point at 100-, 50-, and 10-m levels for station = 03.

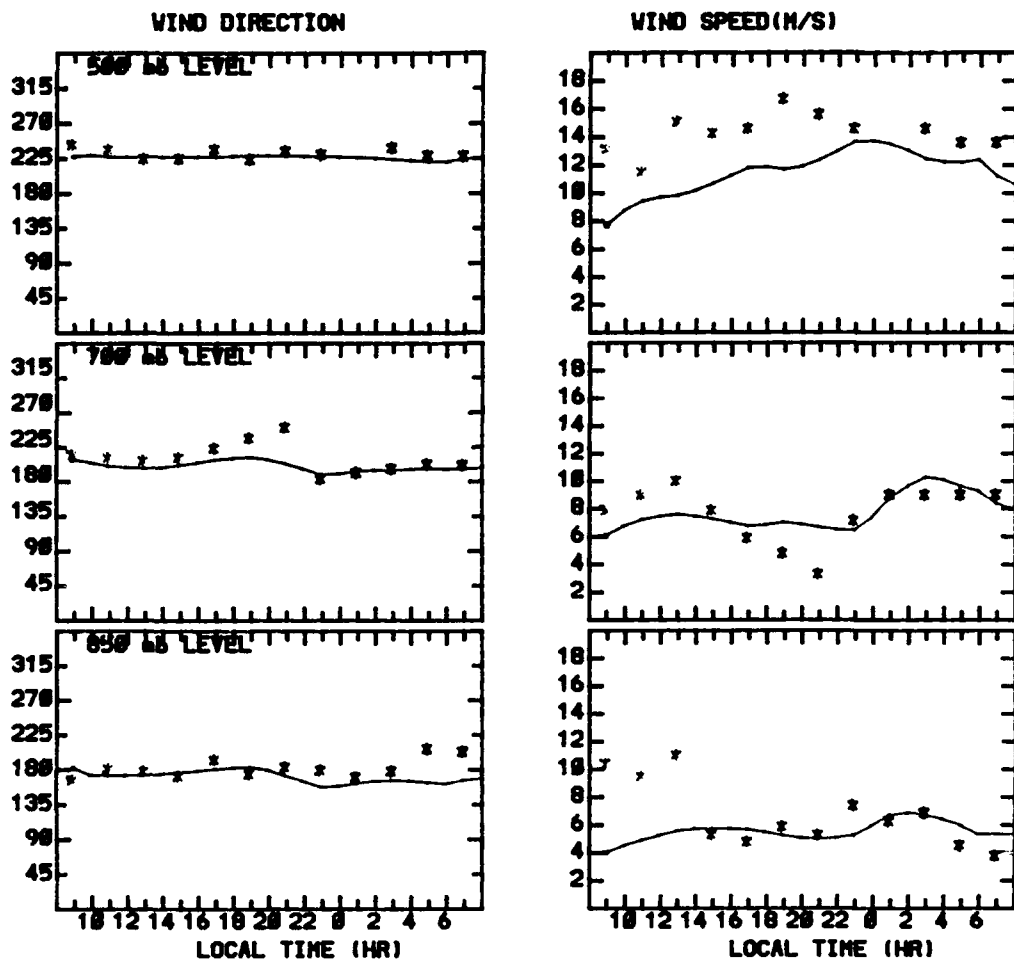


Figure 12. Time series of wind direction and windspeed at 500-, 700-, and 850-mbar levels for station = 03.

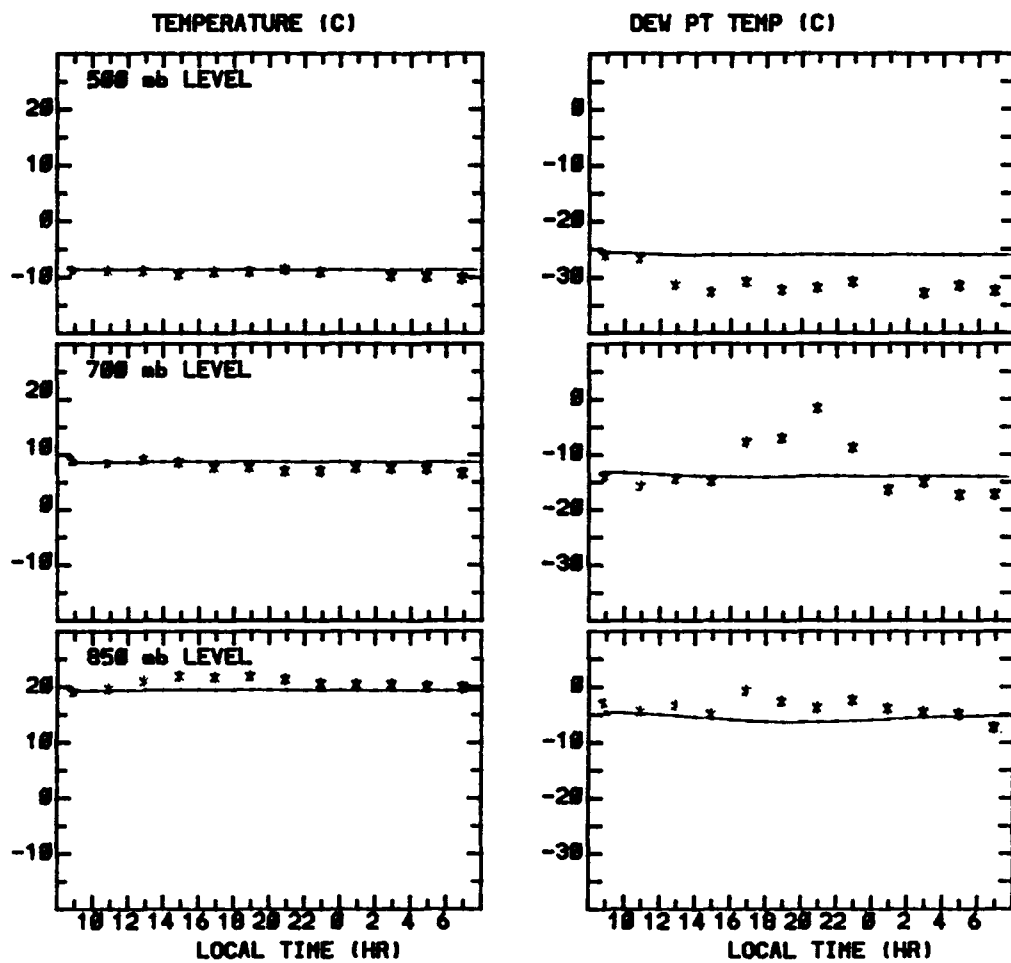


Figure 13. Time series of temperature and dew point at 500-, 700-, and 850-mbar levels for station = 03.

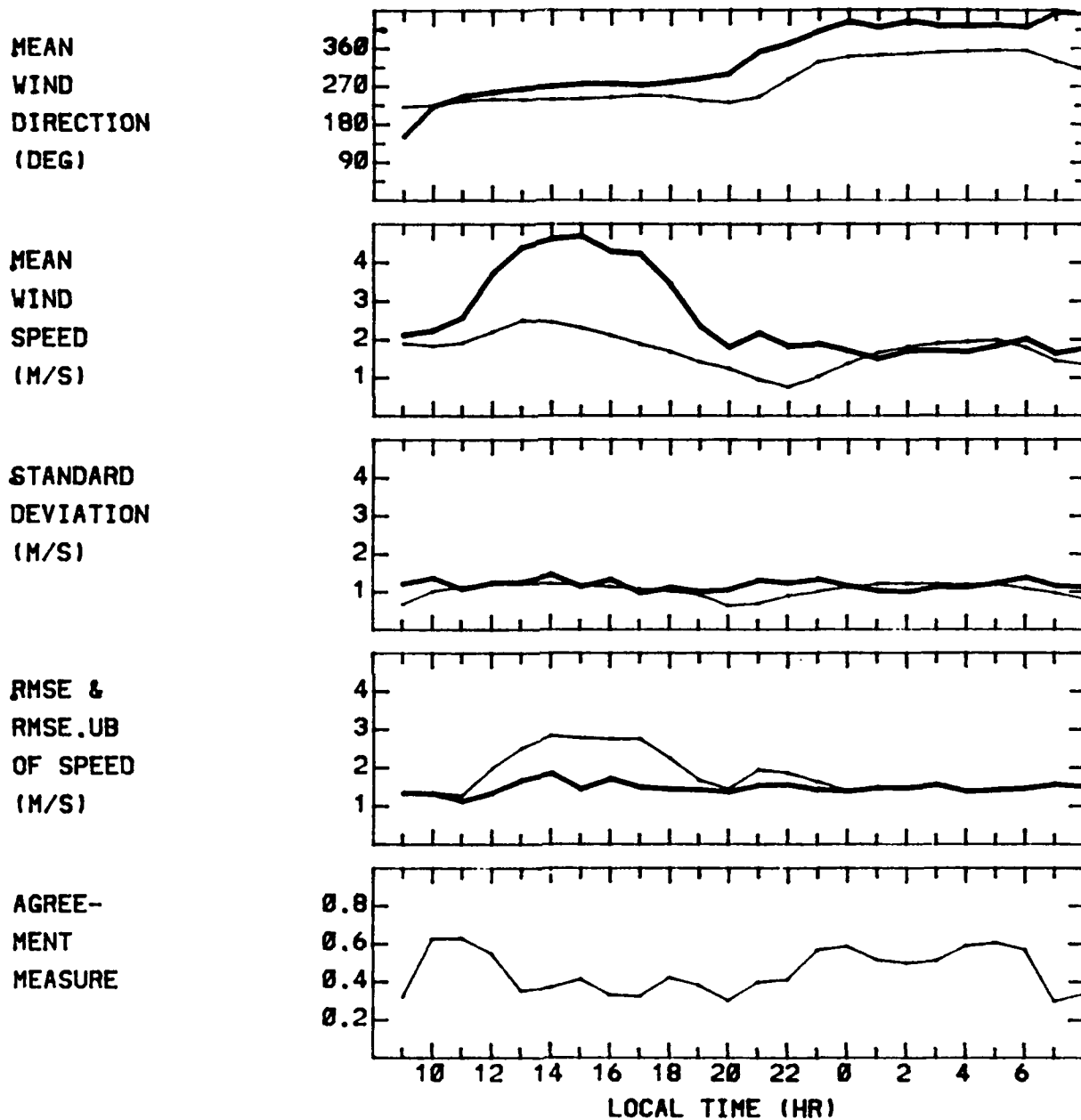
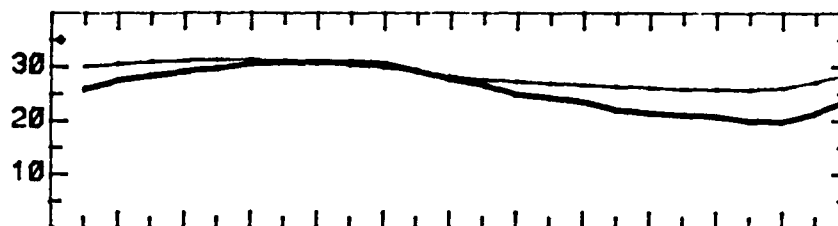
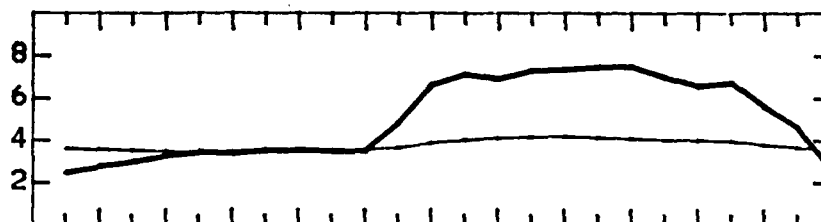


Figure 14. Time series of statistical parameters for surface wind data. Mean wind direction and windspeed, standard deviation, rmse, and agreement measure. In the top three portions of the figure, the thin lines are for simulation and the thick lines are for observation. In the fourth portion (rmse), the thin line is for  $E_b$  and the thick is for  $E_{ub}$ .

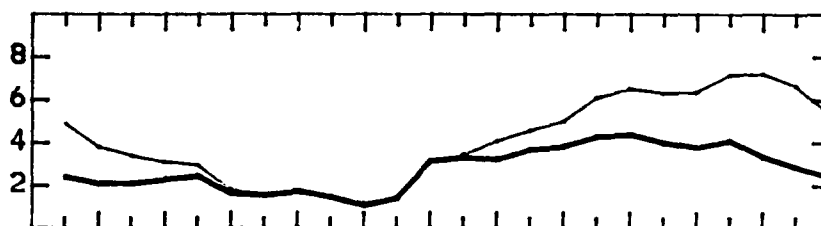
MEAN  
TEMPERATURE  
AT 10 M  
(C)



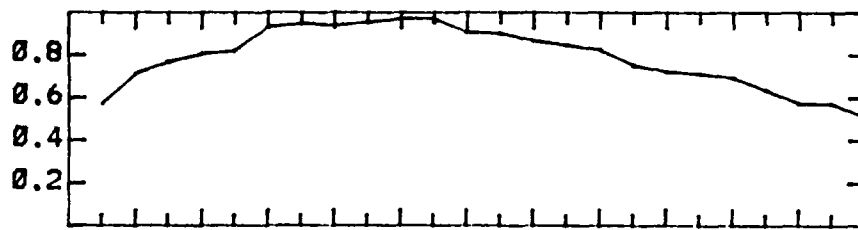
S.D. OF  
TEMPERATURE (C)  
AT 10 M



RMSE &  
RMSE.UB  
OF TEMP. (C)  
AT 10 M



AGREE-  
MENT  
MEASURE



LOCAL TIME (HR)

Figure 15. Time series of statistical parameters for surface (10-m level) temperature. In the top two portions of the figure, the thin lines are for simulation and the thick lines are for observation. In the third portion, the thin line is for  $E_b$  and the thick line is for  $E_{ub}$ .

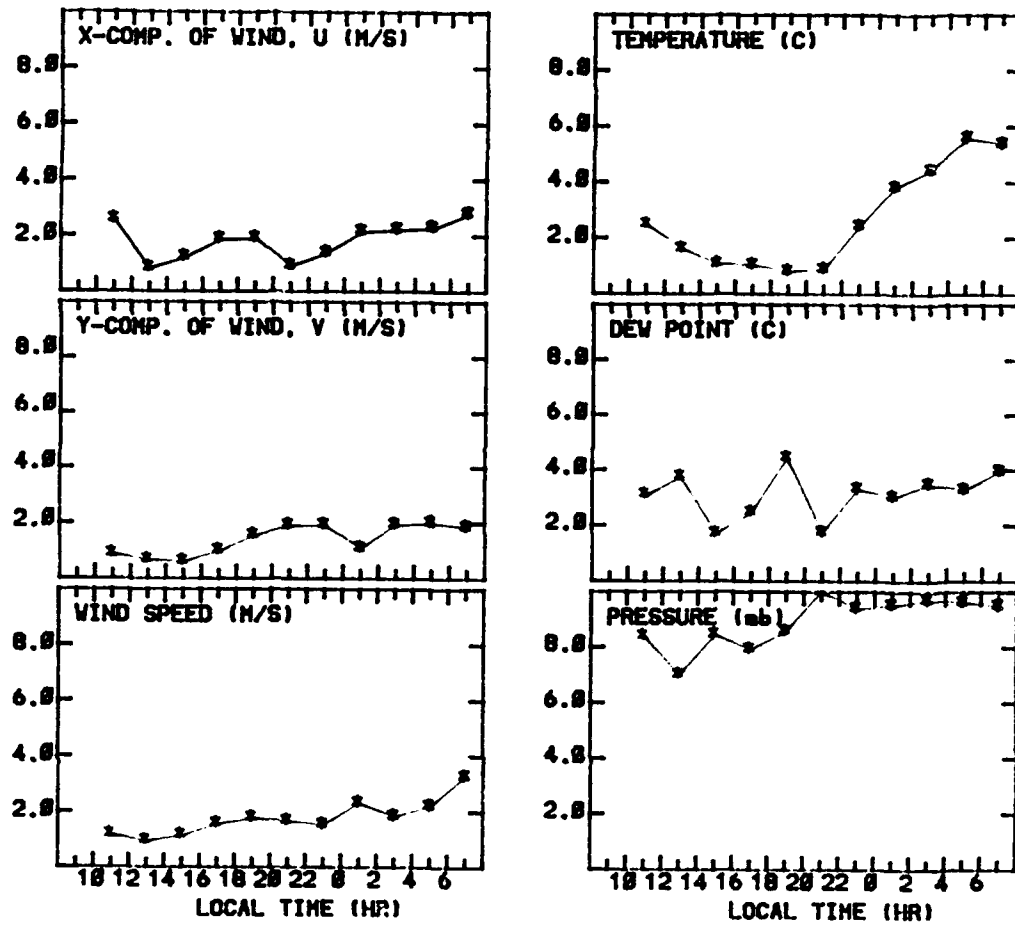


Figure 16. Time series of average differences between observation and simulation for horizontal wind vector components, speed, temperature, dew point, and pressure at the 10-m level.



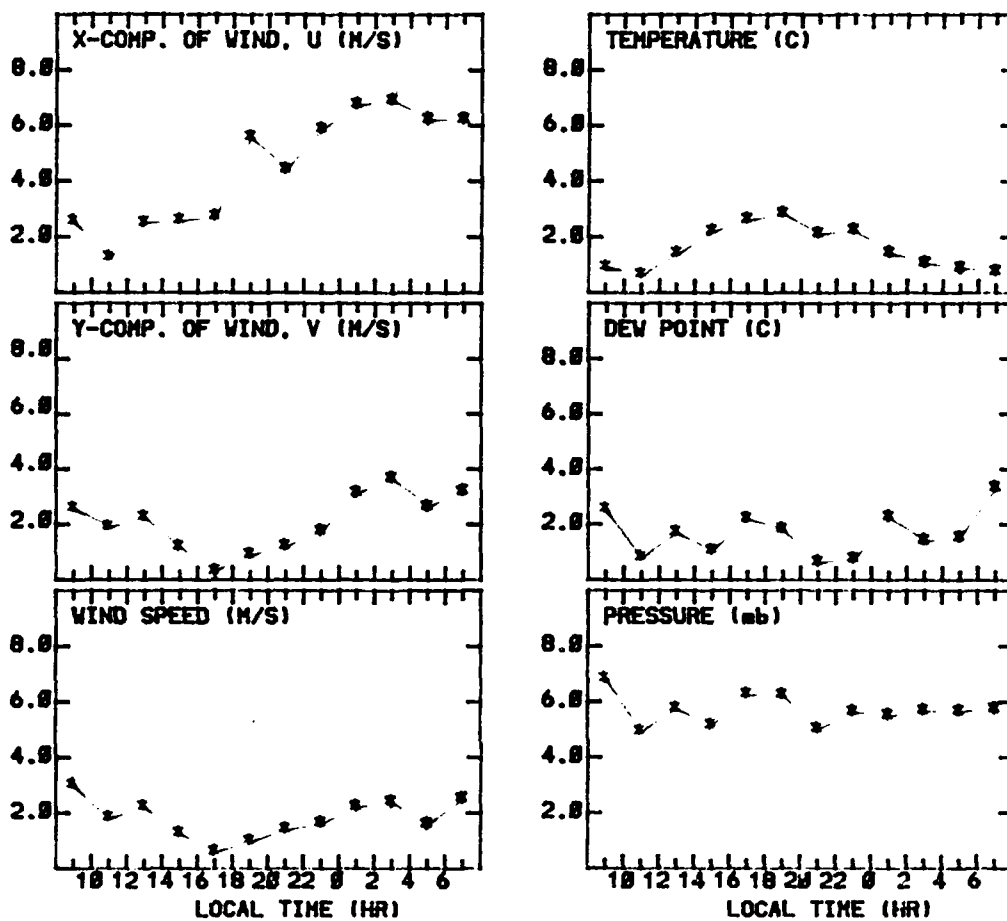


Figure 17. Time series of average differences between observation and simulation for horizontal wind vector components, speed, temperature, dew point, and pressure at the 1000-m level.

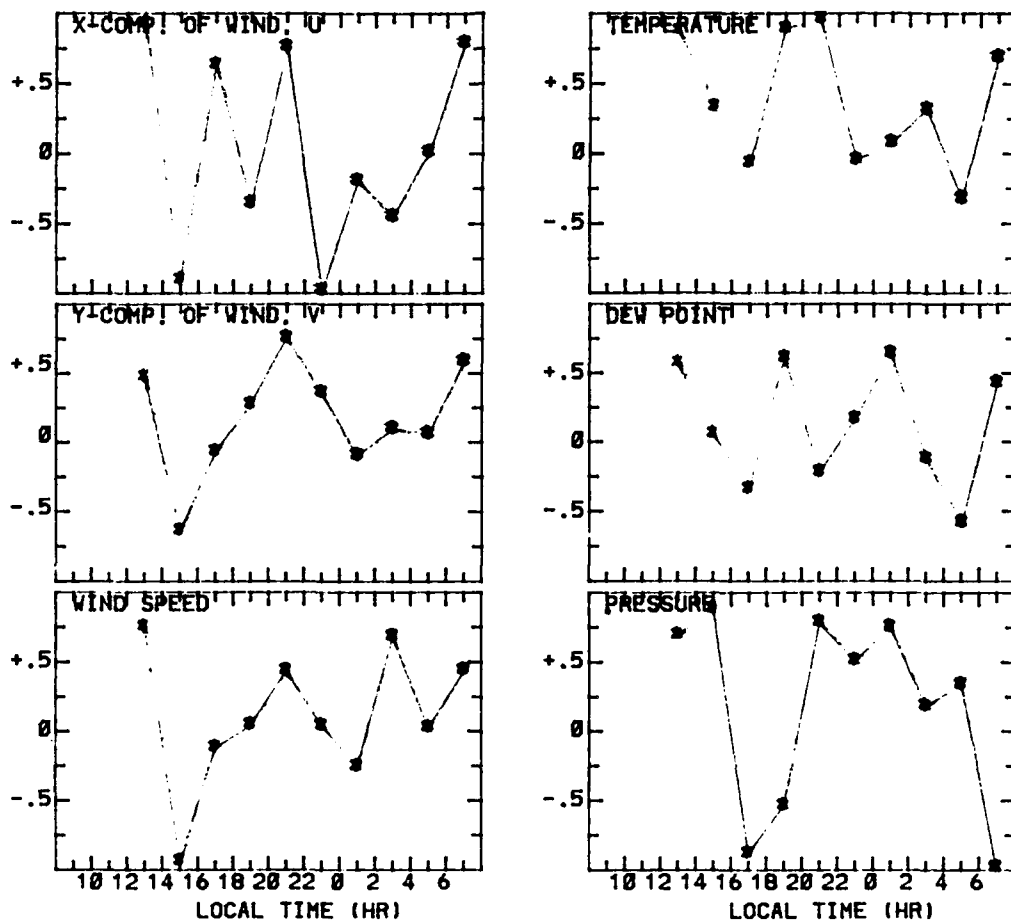


Figure 18. Time series of correlation coefficients of horizontal wind vector components, speed, temperature, dew point, and pressure for the 10-m level.

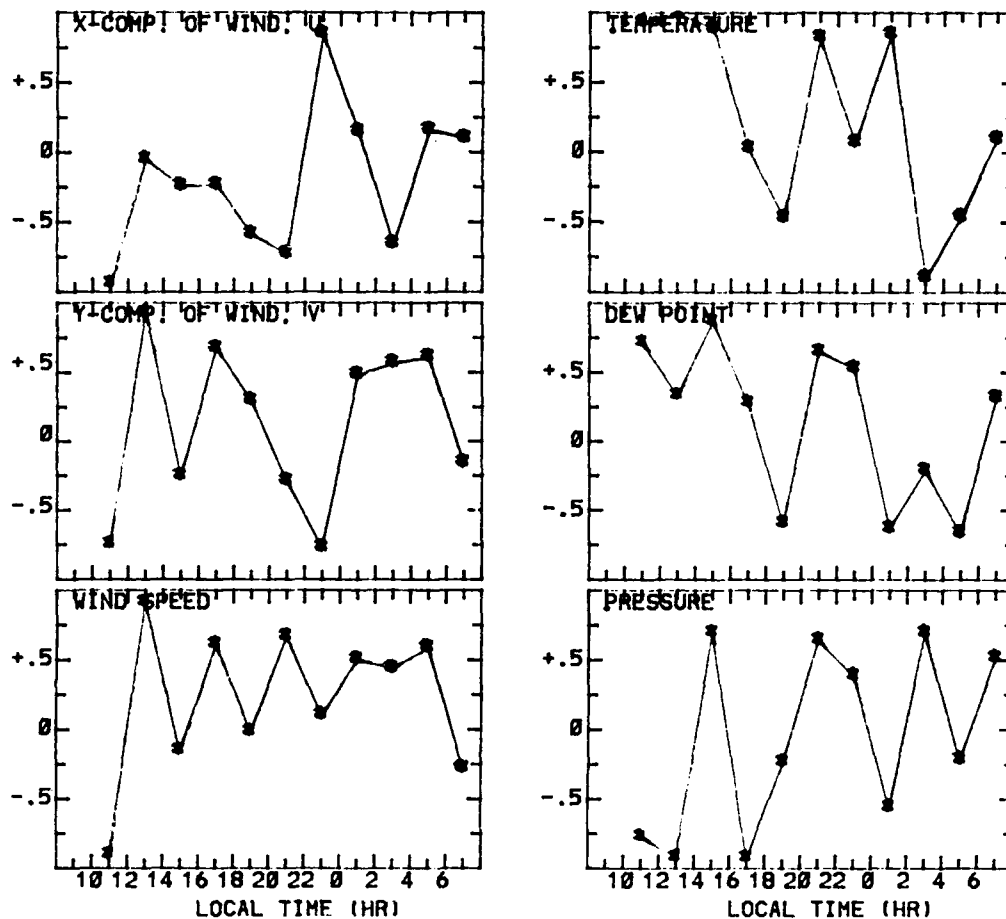


Figure 19. Time series of correlation coefficients of horizontal wind vector components, speed, temperature, dew point, and pressure for the 1000-m level.

#### LITERATURE CITED

- Cionco, R. M., 1990, Project WIND Documentation and User Guide, Phase I: 24-hr period, 0900 PST, 27 June - 0900 hrs PST, 28 June 1985, Internal Report, U.S. Army Atmospheric Sciences Laboratory, White Sands Missile Range, NM.
- Press, W. H., B. P. Flannery, S. A. Teukolsky, and W. T. Vetterling, 1989, "Numerical Recipes," The Art of Scientific Computing (FORTRAN Version), Cambridge University Press, Cambridge, MA.
- Willmott, C. J., 1981, "On the Validation of Models," Physical Geography, 2:168-194.
- Willmott, C. J., 1982, "Some Comments on the Evaluation of Model Performance," Bull Am Meteorol Soc, 63:1309-1313.
- Willmott, C. J., S. G. Ackleston, R. E. Davis, J. J. Feddema, K. M. Klink, D. R. Legates, J. O'Donnell and C. M. Rowe, 1985, Statistics for the Evaluation and Comparison of Models, J Geophys Res, 90(C5):8995-9005.
- Yamada, T., and S. Bunker, 1989, "A Numerical Model Study of Nocturnal Drainage Flows with Strong Wind and Temperature Gradients, J Appl Meteorol, 28:545-554.

DISTRIBUTION LIST FOR PUBLIC RELEASE

Commandant  
U.S. Army Chemical School  
ATTN: ATZN-CM-CC (S. Barnes)  
Fort McClellan, AL 36205-5020

Commander  
U.S. Army Aviation Center  
ATTN: ATZQ-D-MA  
Mr. Oliver N. Heath  
Fort Rucker, AL 36362

Commander  
U.S. Army Aviation Center  
ATTN: ATZQ-D-MS (Mr. Donald Wagner)  
Fort Rucker, AL 36362

NASA/Marshall Space Flight Center  
Deputy Director  
Space Science Laboratory  
Atmospheric Sciences Division  
ATTN: E501 (Dr. George H. Fichtl)  
Huntsville, AL 35802

NASA/Marshall Space Flight Center  
Atmospheric Sciences Division  
ATTN: Code ED-41  
Huntsville, AL 35812

Deputy Commander  
U.S. Army Strategic Defense Command  
ATTN: CSSD-SL-L  
Dr. Julius Q. Lilly  
P.O. Box 1500  
Huntsville, AL 35807-3801

Commander  
U.S. Army Missile Command  
ATTN: AMSMI-RD-AC-AD  
Donald R. Peterson  
Redstone Arsenal, AL 35898-5242

Commander  
U.S. Army Missile Command  
ATTN: AMSMI-RD-AS-SS  
Huey F. Anderson  
Redstone Arsenal, AL 35898-5253

Commander  
U.S. Army Missile Command  
ATTN: AMSMI-RD-AS-SS  
B. Williams  
Redstone Arsenal, AL 35898-5253

Commander  
U.S. Army Missile Command  
ATTN: AMSMI-RD-DE-SE  
Gordon Lill, Jr.  
Redstone Arsenal, AL 35898-5245

Commander  
U.S. Army Missile Command  
Redstone Scientific Information  
Center  
ATTN: AMSMI-RD-CS-R/Documents  
Redstone, Arsenal, AL 35898-5253

Commander  
U.S. Army Intelligence Center  
and Fort Huachuca  
ATTN: ATSI-CDC-C (Mr. Colanto)  
Fort Huachuca, AZ 85613-7000

Northrup Corporation  
Electronics Systems Division  
ATTN: Dr. Richard D. Tooley  
2301 West 120th Street, Box 5032  
Hawthorne, CA 90251-5032

Commander - Code 3331  
Naval Weapons Center  
ATTN: Dr. Alexis Shlanta  
China Lake, CA 93555

Commander  
Pacific Missile Test Center  
Geophysics Division  
ATTN: Code 3250-3 (R. de Violini)  
Point Mugu, CA 93042-5000

Commander  
Pacific Missile Test Center  
Geophysics Division  
ATTN: Code 3250 (Terry E. Battalino)  
Point Mugu, CA 93042-5000

Lockheed Missiles & Space Co., Inc.  
Kenneth R. Hardy  
Org/91-01 B/255  
3251 Hanover Street  
Palo Alto, CA 94304

Commander  
Naval Ocean Systems Center  
ATTN: Code 54 (Dr. Juergen Richter)  
San Diego, CA 92152-5000

Meteorologist in Charge  
Kwajalein Missile Range  
P.O. Box 67  
APO San Francisco, CA 96555

U.S. Department of Commerce  
Mountain Administration Support  
Center  
Library, R-51 Technical Reports  
325 S. Broadway  
Boulder, CO 80303

Dr. Hans J. Liebe  
NTIA/ITS S 3  
325 S. Broadway  
Boulder, CO 80303

NCAR Library Serials  
National Center for Atmos Rsch  
P.O. Box 3000  
Boulder, CO 80307-3000

Bureau of Reclamation  
ATTN: D: 1200  
P.O. Box 25007  
Denver, CO 80225

HQDA  
ODCSOPS  
ATTN: DAMO-FDZ  
Washingting, D.C. 20310-0460

Mil Asst for Env Sci Ofc of  
The Undersecretary of Defense  
for Rsch & Engr/R&AT/E&LS  
Pentagon - Room 3D129  
Washington, D.C. 20301-3080

Director  
Naval Research Laboratory  
ATTN: Code 4110  
Dr. Lothar H. Ruhnke  
Washington, D.C. 20375-5000

HQDA  
DEAN-RMD/Dr. Gomez  
Washington, D.C. 20314

Director  
Division of Atmospheric Science  
National Science Foundation  
ATTN: Dr. Eugene W. Bierly  
1800 G. Street, N.W.  
Washington, D.C. 20550

Commander  
Space & Naval Warfare System Command  
ATTN: PMW-145-1G (LT Painter)  
Washington, D.C. 20362-5100

Commandant  
U.S. Army Infantry  
ATTN: ATSH-CD-CS-OR  
Dr. E. Dutoit  
Fort Benning, GA 30905-5090

USAFETAC/DNE  
Scott AFB, IL 62225

Air Weather Service  
Technical Library - FL4414  
Scott AFB, IL 62225-5458

HQAWS/DOZ  
Scott AFB, IL 62225-5008

USAFETAC/DNE  
ATTN: Mr. Charles Glauber  
Scott AFB, IL 62225-5008

Commander  
U.S. Army Combined Arms Combat  
ATTN: ATZL-CAW (LTC A. Kyle)  
Fort Leavenworth, KS 66027-5300

Commander  
U.S. Army Combined Arms Combat  
ATTN: ATZL-CDB-A (Mr. Annett)  
Fort Leavenworth, KS 66027-5300

Commander  
Phillips Lab  
ATTN: PL/LYP (Mr. Chisholm)  
Hanscom AFB, MA 01731-5000

Director  
Atmospheric Sciences Division  
Geophysics Directorate  
Phillips Lab  
ATTN: Dr. Robert A. McClatchey  
Hanscom AFB, MA 01731-5000

Raytheon Company  
Dr. Charles M. Sonnenschein  
Equipment Division  
528 Boston Post Road  
Sudbury, MA 01776  
Mail Stop 1K9

Director  
U.S. Army Materiel Systems  
Analysis Activity  
ATTN: AMXSY-MP (H. Cohen)  
APG, MD 21005-5071

Commander  
U.S. Army Chemical Rsch,  
Dev & Engr Center  
ATTN: SMCCR-OPA (Ronald Pennsyle)  
APG, MD 21010-5423

Commander  
U.S. Army Chemical Rsch,  
Dev & Engr Center  
ATTN: SMCCR-RS (Mr. Joseph Vervier)  
APG, MD 21010-5423

Commander  
U.S. Army Chemical Rsch,  
Dev & Engr Center  
ATTN: SMCCR-MUC (Mr. A. Van De Wal)  
APG, MD 21010-5423

Director  
U.S. Army Materiel Systems  
Analysis Activity  
ATTN: AMXSY-AT (Mr. Fred Campbell)  
APG, MD 21005-5071

Director  
U.S. Army Materiel Systems  
Analysis Activity  
ATTN: AMXSY-CR (Robert N. Marchetti)  
APG, MD 21005-5071

Director  
U.S. Army Materiel Systems  
Analysis Activity  
ATTN: AMXSY-CS (Mr. Brad W. Bradley)  
APG, MD 21005-5071

Commander  
U.S. Army Laboratory Command  
ATTN: AMSLC-CG  
2800 Powder Mill Road  
Adelphi, MD 20783-1145

Commander  
Headquarters  
U.S. Army Laboratory Command  
ATTN: AMSLC-CT  
2800 Powder Mill Road  
Adelphi, MD 20783-1145

Commander  
Harry Diamond Laboratories  
ATTN: SLCIS-CO  
2800 Powder Mill Road  
Adelphi, MD 20783-1197

Director  
Harry Diamond Laboratories  
ATTN: SLCHD-ST-SP  
Dr. Z.G. Sztankay  
Adelphi, MD 20783-1197

AFMC/DOW  
Wright-Patterson AFB, OH 0334-5000

National Security Agency  
ATTN: W21 (Dr. Longbothum)  
9800 Savage Road  
Ft George G. Meade, MD 20755-6000

U. S. Army Space Technology  
and Research Office  
ATTN: Brenda Brathwaite  
5321 Riggs Road  
Gaithersburg, MD 20882

Officer in Charge  
Naval Surface Weapons Center  
White Oak Library  
Technical Library  
Silver Springs, MD 20910-1090

The Environmental Research  
Institute of MI  
ATTN: IRIA Library  
P.O. Box 8618  
Ann Arbor, MI 48107-8618

Commander  
U.S. Army Research Office  
ATTN: DRXRO-GS (Dr. W.A. Flood)  
P.O. Box 12211  
Research Triangle Park, NC 27709

Dr. Jerry Davis  
North Carolina State University  
Department of Marine, Earth, &  
Atmospheric Sciences  
P.O. Box 8208  
Raleigh, NC 27650-8208

Commander  
U.S. Army Cold Regions Research  
& Engineering Laboratory  
ATTN: CRREL-RG (Mr. Robert Redfield)  
Hanover, NH 03755-1290

Commander  
U.S. Army Cold Regions Research  
& Engineering Laboratory  
ATTN: CECRL-RD (Dr. K.F. Sterrett)  
Hanover, NH 03755-1290

Commanding Officer  
U.S. Army Armament R&D Command  
ATTN: DRDAR-TSS, Bldg 59  
Dover, NJ 07801

U.S. Army Communications-Electronics  
Command Center for EW/RSTA  
ATTN: AMSEL-RD-EW-SP  
Fort Monmouth, NJ 07703-5303

Commander  
U.S. Army Communications-Electronics  
Command  
ATTN: AMSEL-EW-D (File Copy)  
Fort Monmouth, NJ 07703-5303

Headquarters  
U.S. Army Communications-Electronics  
Command  
ATTN: AMSEL-EW-MD  
Fort Monmouth, NJ 07703-5303

Commander  
U.S. Army Satellite Comm Agency  
ATTN: DRCPM-SC-3  
Fort Monmouth, NJ 07703-5303

Director  
EW/RSTA Center  
ATTN: AMSEL-EW-DR  
Fort Monmouth, NJ 07703-5303

USACECOM  
Center for EW/RSTA  
ATTN: AMSEL-RD-EW-SP  
Fort Monmouth, NJ 07703-5303

6585th TG (AFSC)  
ATTN: RX (CPT Stein)  
Holloman AFB, NM 88330

Department of the Air Force  
OL/A 2nd Weather Squadron (MAC)  
Holloman AFB, NM 88330-5000

PL/WE  
Kirtland AFB, NM 87118-6008

Director  
U.S. Army TRADOC Analysis Command  
ATTN: ATRC-WSS-R  
White Sands Missile Range, NM 88002

Rome Laboratory  
ATTN: Technical Library RL/DOVL  
Griffiss AFB, NY 13441-5700

Department of the Air Force  
7th Squadron  
APO, NY 09403

AWS  
USAREUR/AEAWX  
APO, NY 09403-5000



AF Wright Aeronautical Laboratories  
Avionics Laboratory  
ATTN: AFWAL/AARI (Dr. V. Chmelis)  
Wright-Patterson AFB, OH 45433

Commander  
U.S. Army Field Artillery School  
ATTN: ATSF-F-FD (Mr. Gullion)  
Fort Sill, OK 73503-5600

Commandant  
U.S. Army Field Artillery School  
ATTN: ATSF-TSM-TA  
Mr. Charles Taylor  
Fort Sill, OK 73503-5600

Commander  
Naval Air Development Center  
ATTN: Al Salik (Code 5012)  
Warminster, PA 18974

Commander  
U.S. Army Dugway Proving Ground  
ATTN: STEDP-MT-DA-M  
Mr. Paul Carlson  
Dugway, UT 84022

Commander  
U.S. Army Dugway Proving Ground  
ATTN: STEDP-MT-DA-L  
Dugway, UT 84022

Commander  
U.S. Army Dugway Proving Ground  
ATTN: STEDP-MT-M (Mr. Bowers)  
Dugway, UT 84022-5000

Defense Technical Information Center  
ATTN: DTIC-FDAC  
Cameron Station  
Alexandria, VA 22314

Commanding Officer  
U.S. Army Foreign Science &  
Technology Center  
ATTN: CM  
220 7th Street, NE  
Charlottesville, VA 22901-5396

Naval Surface Weapons Center  
Code G63  
Dahlgren, VA 22448-5000

Commander  
U.S. Army OEC  
ATTN: CSTE-EFS  
Park Center IV  
4501 Ford Ave  
Alexandria, VA 22302-1458

Commander and Director  
U.S. Army Corps of Engineers  
Engineer Topographics Laboratory  
ATTN: ETL-GS-LB  
Fort Belvoir, VA 22060

Department of the Air Force  
HQ 5 Weather Wing (MAC)  
ATTN: 5 WW/DN  
Langley AFB, VA 23665-5000

Commander and Director  
U.S. Army Corps of Engineers  
Engineer Topographics Laboratory  
ATTN: CEETL-ZD  
Fort Belvoir, VA 22060-5546

Commander  
Logistics Center  
ATTN: ATCL-CE  
Fort Lee, VA 23801-6000

Commander  
USATRADO  
ATTN: ATCD-FA  
Fort Monroe, VA 23651-5170

Science and Technology  
101 Research Drive  
Hampton, VA 23666-1340

Commander  
U.S. Army Nuclear & Cml Agency  
ATTN: MONA-ZB Bldg 2073  
Springfield, VA 22150-3198